

**PHY 711 Classical Mechanics and
Mathematical Methods
10-10:50 AM MWF Olin 103**

Plan for Lecture 38

- 1. Chapter 12: Example of solution to Navier-Stokes equation**
- 2. Chapter 13: Physics of elastic continua**

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23	Mon, 10/20/2014	Appendix A	Fourier transforms	#16
24	Wed, 10/22/2014	Chap. 5	Motion of Rigid Bodies	#17
25	Fri, 10/24/2014	Chap. 5	Motion of Rigid Bodies	#18
26	Mon, 10/27/2014	Chap. 5	Symmetric top in gravitational field	#18
27	Wed, 10/29/2014	Chap. 8	Vibrations of membranes	#19
28	Fri, 10/31/2014	Chap. 9	Physics of fluids	#20
29	Mon, 11/03/2014	Chap. 9	Physics of fluids	#21
30	Wed, 11/05/2014	Chap. 9	Sound waves	
31	Fri, 11/07/2014	Chap. 9	Sound waves	Begin Take-Home
32	Mon, 11/10/2014	Chap. 9	Non-linear effects	Continue Take-Home
33	Wed, 11/12/2014	Chap. 10	Surface waves in fluids	Continue Take-Home
34	Fri, 11/14/2014	Chap. 10	Surface waves in fluids	Continue Take-Home
35	Mon, 11/17/2014	Chap. 11	Heat Conduction	Take-Home due #22
36	Wed, 11/19/2014	Chap. 12	Viscosity	#23
37	Fri, 11/21/2014	Chap. 12	More viscosity	#24
38	Mon, 11/24/2014	Chap. 13	Elastic Continua	Prepare presentations
	Wed, 11/26/2014		Thanksgiving Holiday	
	Fri, 11/28/2014		Thanksgiving Holiday	
39	Mon, 12/01/2014	Chap. 13	Elastic Continua	Prepare presentations
	Wed, 12/03/2014		Student presentations I	
	Fri, 12/05/2014		Student presentations II	
	Mon, 12/08/2014		Begin Take-home final	Final grades due 12/17/2014

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Signup for PHY 711 Presentations

Wed. December 3, 2014

Time	Name	Title
10:00 AM	Lauren Nelson	
10:25 AM		

Fri. December 5, 2014

Time	Name	Title
10:00 AM		
10:25 AM		

Please sign up

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Newton-Euler equations for viscous fluids

Navier-Stokes equation

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \frac{1}{\rho} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \mathbf{v})$$

Continuity condition

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

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Example – steady flow of an incompressible fluid in a long pipe with a circular cross section of radius R

Navier-Stokes equation

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \frac{1}{\rho} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \mathbf{v})$$

Continuity condition

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

Incompressible fluid $\Rightarrow \nabla \cdot \mathbf{v} = 0$

$$\text{Steady flow} \Rightarrow \frac{\partial \mathbf{v}}{\partial t} = 0$$

$$\text{Irrotational flow} \Rightarrow \nabla \times \mathbf{v} = 0$$

$$\text{No applied force} \Rightarrow \mathbf{f} = 0$$

$$\text{Neglect non-linear terms} \Rightarrow \nabla(v^2) = 0$$

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Example – steady flow of an incompressible fluid in a long pipe with a circular cross section of radius R -- continued

Navier-Stokes equation becomes:

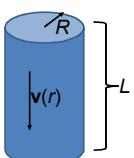
$$0 = -\frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v}$$

$$\text{Assume that } \mathbf{v}(r, t) = v_z(r) \hat{\mathbf{z}}$$

$$\frac{\partial p}{\partial z} = \eta \nabla^2 v_z(r) \quad (\text{independent of } z)$$

$$\text{Suppose that } \frac{\partial p}{\partial z} = -\frac{\Delta p}{L}$$

$$\Rightarrow \nabla^2 v_z(r) = -\frac{\Delta p}{\eta L}$$



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Example – steady flow of an incompressible fluid in a long pipe with a circular cross section of radius R -- continued

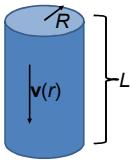
$$\nabla^2 v_z(r) = -\frac{\Delta p}{\eta L}$$

$$\frac{1}{r} \frac{d}{dr} r \frac{dv_z(r)}{dr} = -\frac{\Delta p}{\eta L}$$

$$v_z(r) = -\frac{\Delta p r^2}{4\eta L} + C_1 \ln(r) + C_2$$

$$\Rightarrow C_1 = 0 \quad v_z(R) = 0 = -\frac{\Delta p R^2}{4\eta L} + C_2$$

$$v_z(r) = \frac{\Delta p}{4\eta L} (R^2 - r^2)$$



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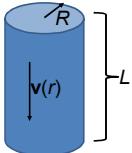
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Example – steady flow of an incompressible fluid in a long pipe with a circular cross section of radius R -- continued

$$v_z(r) = \frac{\Delta p}{4\eta L} (R^2 - r^2)$$

Mass flow rate through the pipe:

$$\frac{dM}{dt} = 2\pi\rho \int_0^R r dr v_z(r) = \frac{\Delta p \rho \pi R^4}{8\eta L}$$



Poiseuille formula;
→ Method for measuring η

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Newton-Euler equations for viscous fluids – effects on sound

Recall full equations:

Navier-Stokes equation

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \frac{1}{\rho} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \mathbf{v})$$

Continuity condition

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

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Newton-Euler equations for viscous fluids – effects on sound

Without viscosity terms:

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p \quad \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

Assume: $\mathbf{v} = \mathbf{0} + \delta \mathbf{v}$ $\mathbf{f} = \mathbf{0}$ $\rho = \rho_0 + \delta \rho$

$$p = p_0 + \delta p = p_0 + c^2 \delta \rho$$

Linearized equations: $\frac{\partial \delta \mathbf{v}}{\partial t} = -\frac{c^2}{\rho_0} \nabla \delta \rho \quad \frac{\partial \delta \rho}{\partial t} + \rho_0 \nabla \cdot (\delta \mathbf{v}) = 0$

Let $\delta \mathbf{v} \equiv \delta \mathbf{v}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ $\delta \rho \equiv \delta \rho_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$

$$\Rightarrow \omega \delta \mathbf{v}_0 = \frac{c^2 \delta \rho_0}{\rho_0} \mathbf{k} \quad -\omega \delta \rho_0 + \rho_0 \mathbf{k} \cdot \delta \mathbf{v}_0 = 0$$

$$\Rightarrow k^2 = \frac{\omega^2}{c^2} \quad \frac{\delta \rho_0}{\rho_0} = \frac{\mathbf{k} \cdot \delta \mathbf{v}_0}{c}$$

→ Pure longitudinal harmonic wave solutions

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Newton-Euler equations for viscous fluids – effects on sound
Recall full equations:

Navier-Stokes equation

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \frac{1}{\rho} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \mathbf{v})$$

Continuity condition

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

Assume: $\mathbf{v} = \mathbf{0} + \delta \mathbf{v}$ $\mathbf{f} = \mathbf{0}$ $\rho = \rho_0 + \delta \rho$

$$p = p_0 + \delta p = p_0 + c^2 \delta \rho + \left(\frac{\partial p}{\partial s} \right)_\rho \delta s$$

$$\text{where } c^2 \equiv \left(\frac{\partial p}{\partial \rho} \right)_s$$

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Newton-Euler equations for viscous fluids – effects on sound
Note that pressure now depends both on density and entropy so that entropy must be coupled into the equations

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{f} - \frac{1}{\rho} \nabla p + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \frac{1}{\rho} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \mathbf{v})$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0 \quad \rho T \frac{\partial s}{\partial t} = k_{th} \nabla^2 T$$

Assume: $\mathbf{v} = \mathbf{0} + \delta \mathbf{v}$ $\mathbf{f} = \mathbf{0}$ $\rho = \rho_0 + \delta \rho$

$$p = p_0 + \delta p = p_0 + c^2 \delta \rho + \left(\frac{\partial p}{\partial s} \right)_\rho \delta s \quad \text{where } c^2 \equiv \left(\frac{\partial p}{\partial \rho} \right)_s$$

$$T = T_0 + \delta T = T_0 + \left(\frac{\partial T}{\partial \rho} \right)_s \delta \rho + \left(\frac{\partial T}{\partial s} \right)_\rho \delta s$$

$$s = s_0 + \delta s$$

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Newton-Euler equations for viscous fluids – effects on sound
Linearized equations (with the help of various thermodynamic relationships):

$$\frac{\partial \delta \mathbf{v}}{\partial t} = -\frac{c^2}{\rho_0} \nabla \delta \rho - \rho_0 \left(\frac{\partial T}{\partial \rho} \right)_s \nabla \delta s + \frac{\eta}{\rho_0} \nabla^2 \delta \mathbf{v} + \frac{1}{\rho_0} \left(\zeta + \frac{1}{3} \eta \right) \nabla (\nabla \cdot \delta \mathbf{v})$$

$$\frac{\partial \delta \rho}{\partial t} + \rho_0 \nabla \cdot (\delta \mathbf{v}) = 0$$

$$\frac{\partial \delta s}{\partial t} = \gamma \kappa \nabla^2 \delta s + \frac{c_p \kappa}{T_0} \left(\frac{\partial T}{\partial \rho} \right)_s \nabla^2 \delta \rho$$

Here: $\gamma = \frac{c_p}{c_v}$ $\kappa = \frac{k_{th}}{c_p \rho_0}$

Let $\delta \mathbf{v} \equiv \delta \mathbf{v}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ $\delta \rho \equiv \delta \rho_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ $\delta s \equiv \delta s_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$

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Newton-Euler equations for viscous fluids – effects on sound
Linearized plane wave solutions:

$$\omega \delta \mathbf{v}_0 = -\frac{c^2 \delta \rho_0}{\rho_0} \mathbf{k} - \rho_0 \left(\frac{\partial T}{\partial \rho} \right)_s \delta s_0 \mathbf{k} - \frac{i \eta k^2}{\rho_0} \delta \mathbf{v}_0 - \frac{i}{\rho_0} \left(\zeta + \frac{1}{3} \eta \right) \mathbf{k} (\mathbf{k} \cdot \delta \mathbf{v}_0)$$

$$\frac{\partial \delta \rho_0}{\partial t} - \rho_0 \mathbf{k} \cdot \delta \mathbf{v}_0 = 0$$

$$\omega \delta s_0 = -i \gamma \kappa k^2 \delta s_0 - \frac{i c_p \kappa}{T_0} \left(\frac{\partial T}{\partial \rho} \right)_s k^2 \delta \rho_0$$

Longitudinal solutions:

$$\left(\omega^2 - c^2 k^2 + i \frac{\omega k^2}{\rho_0} \left(\frac{4}{3} \eta + \zeta \right) \right) \delta \rho_0 - \rho_0^2 k^2 \left(\frac{\partial T}{\partial \rho} \right)_s \delta s_0 = 0$$

$$\frac{i c_p \kappa k^2}{T_0} \left(\frac{\partial T}{\partial \rho} \right)_s \delta \rho_0 + (\omega + i \gamma \kappa k^2) \delta s_0 = 0$$

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Newton-Euler equations for viscous fluids – effects on sound
Linearized plane wave longitudinal solutions:

Longitudinal solutions:

$$\left(\omega^2 - c^2 k^2 + i \frac{\omega k^2}{\rho_0} \left(\frac{4}{3} \eta + \zeta \right) \right) \delta \rho_0 - \rho_0^2 k^2 \left(\frac{\partial T}{\partial \rho} \right)_s \delta s_0 = 0$$

$$\frac{i c_p \kappa k^2}{T_0} \left(\frac{\partial T}{\partial \rho} \right)_s \delta \rho_0 + (\omega + i \gamma \kappa k^2) \delta s_0 = 0$$

Approximate solution: $k = \frac{\omega}{c} + i\alpha$

where $\alpha \approx \frac{\omega^2}{2c^3 \rho_0} \left(\frac{4}{3} \eta + \zeta \right) + \frac{\kappa c_p \rho_0^2 \omega^2}{2T_0 c^5} \left(\frac{\partial T}{\partial \rho} \right)^2$

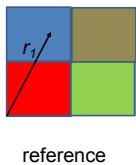
$$\delta \rho = \delta \rho_0 e^{-\alpha \mathbf{k} \cdot \mathbf{r}} e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$$

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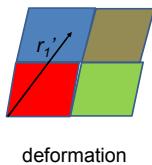
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Brief introduction to elastic continua



reference



deformation

$$\mathbf{r}_1' = \mathbf{r}_1 + \mathbf{u}(\mathbf{r}_1) \quad \mathbf{r}_2' = \mathbf{r}_2 + \mathbf{u}(\mathbf{r}_2)$$

$$\mathbf{r}_2' - \mathbf{r}_1' = \mathbf{r}_2 - \mathbf{r}_1 + ((\mathbf{r}_2 - \mathbf{r}_1) \cdot \nabla) \mathbf{u}(\mathbf{r}_1)$$

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Brief introduction to elastic continua

Deformation components:

$$\frac{\partial u_i}{\partial x_j} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$

$$\equiv \epsilon_{ij} + O_{ij}$$

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To be continued

Have a great Thanksgiving Holiday.

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